



Picking the right parameters

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Slides courtesy of Jack Radcliffe (SARAO/Pretoria)



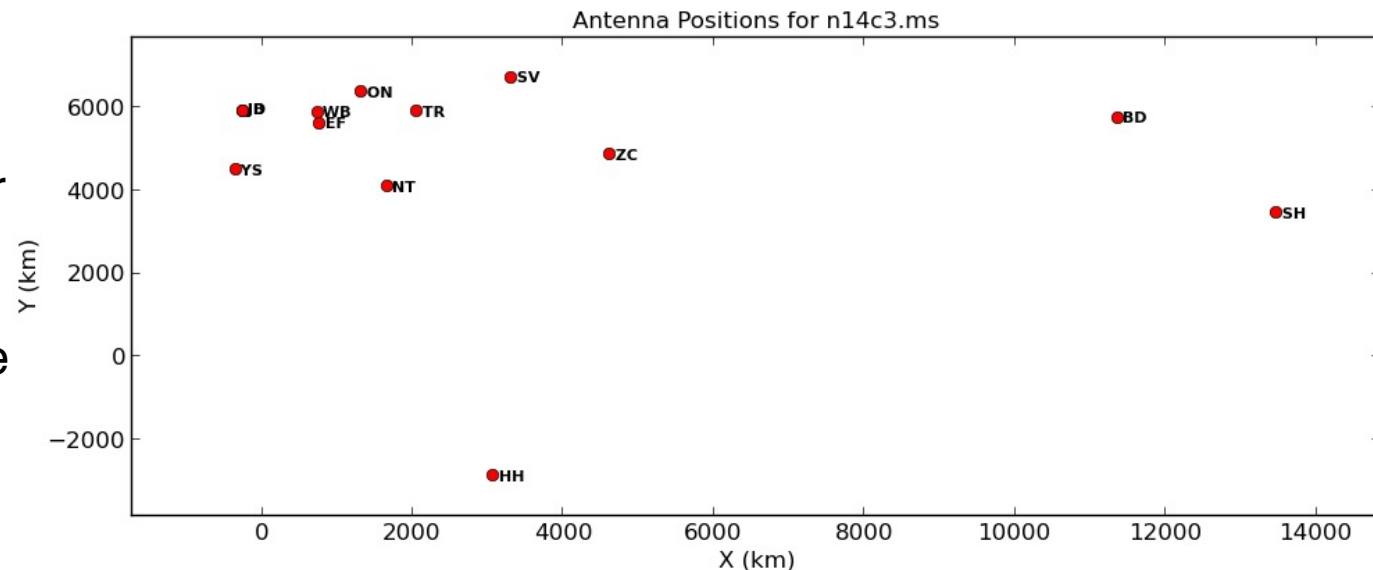
Summary

- **How do you know what parameters to set, and what do you set them to?**
- Some are standard e.g. `vis='?'`, but others e.g. phase reference solution interval can affect calibration profusely!
- This lecture should give you some intuition on what to set.

Reference antennas

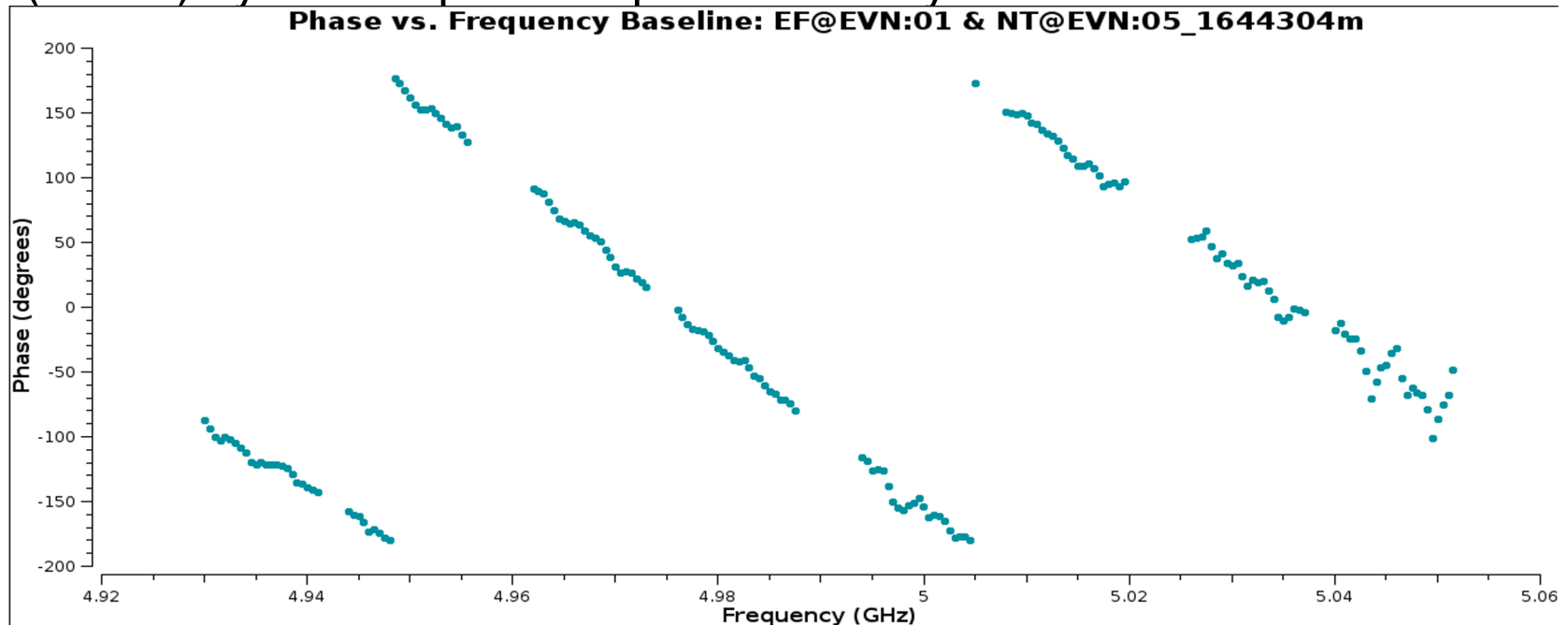
- The reference antenna is the antenna which we compare our solutions too (interferometers only care about relative differences)
- A good reference antenna should be the one that will have the **most good solutions to all other baselines**.
- This means it typically is one or both of:
 - Close to the centre of the array (i.e. lots of short baselines)
 - Or has a large collecting area

Effelsberg is used for the EVN as it's both close to the centre **and** the largest in the EVN (100m)



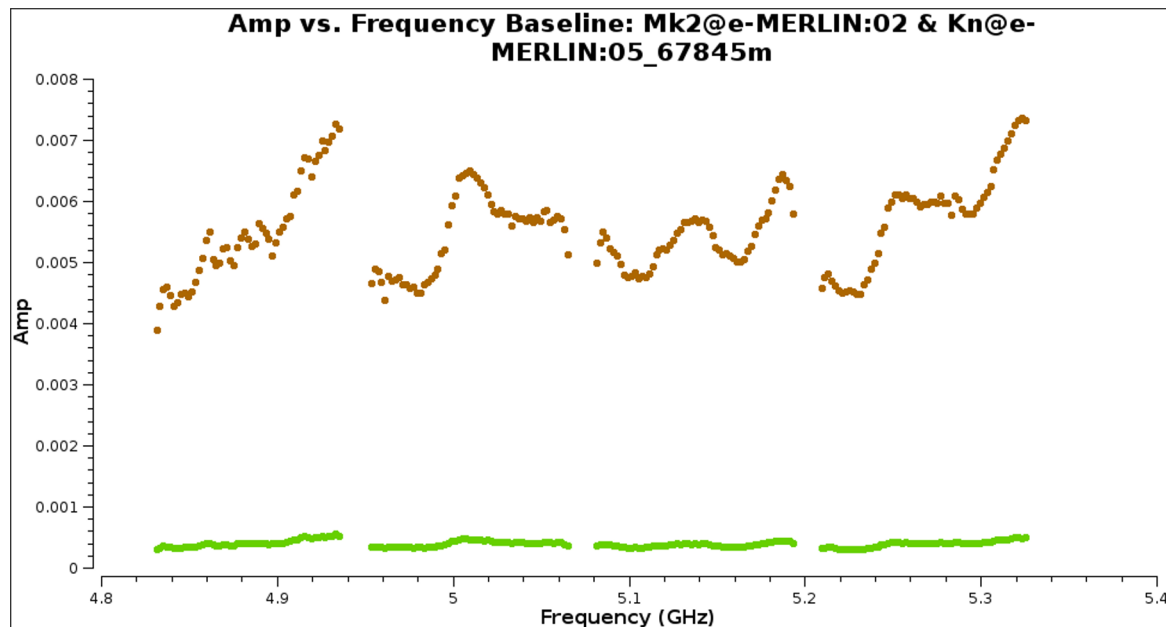
Fringe fitting / delay calibration

- Fits for linear phase gradients
- Inspect phase v. frequency plot
- Can set a delay window – speeds up algorithm
- Delays are usually stable for hours but averaging solint limited (~scan) by time-dependent phase stability

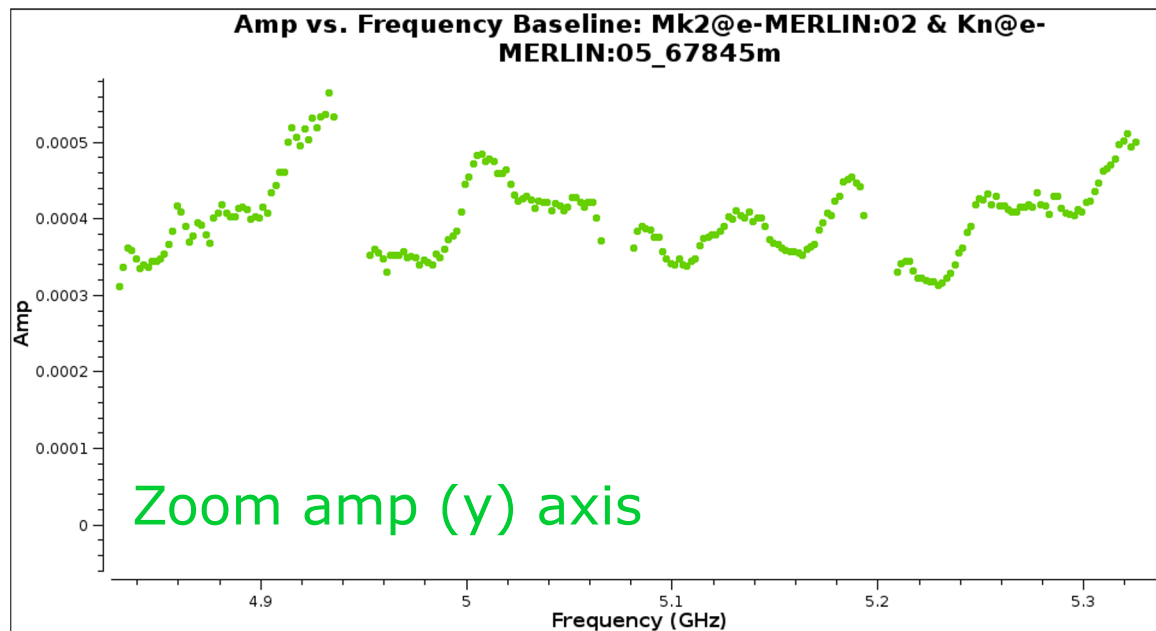


Bandpass calibration

- Correct BP calibrator phase v. time first
- In bandpass, average in time for as long as possible for best S/N per channel
- Example below: Both BP calibrators have same amplitude wiggles
- Could combine, interpolate or use just the one with best S/N?



Bandpass calibration



Additional points

- Normalise bandpass solutions (otherwise flux scale may differ or be unset)
- May need to select timeranges if there's bad data around.

Noise

$$T_{\text{sys}} = \frac{1}{\eta_A e^{-\tau_{\text{atm}}}} \left[T_{\text{Rx}} + \eta_A T_{\text{sky}} + (1 - \eta_A) T_{\text{amb}} \right]$$

$$\sigma_{\text{sys}} = \frac{\langle T_{\text{sys}} \rangle}{\eta_A A_{\text{eff}} \sqrt{(N(N-1)/2) \Delta\nu \Delta t N_{\text{pol}}}}$$

- Lowest possible noise is 'thermal' limit based on T_{sys} (assuming natural weighting).
- Good rule of thumb is that you should **at least reach 3 times the predicted noise floor**.
- So you can only improve on this by:
 - Bigger/more efficient antennas (A_{eff}, η_A) or more (N)
 - Lower noise, R_{X} and/or T_{sky} (observing conditions)
 - Observe for longer/wider bandwidth

Dynamic range

Dynamic range

ATCA simulation • 1.5D config • 12 hour observation
1.5 GHz • 8 × 16 MHz channels • SEFD = 363 Jy

$$\sigma = 27 \mu\text{Jy} / \text{beam}$$



$$P = 2 \text{ Jy}$$

$$DR = \frac{P}{\sigma} = \frac{2}{2.7 \times 10^{-5}} = 74074$$

Deconvolved image

Dynamic range

Dynamic range: alternative definition

ATCA simulation • 1.5D config • 12 hour observation
1.5 GHz • 8 × 16 MHz channels • SEFD = 363 Jy

$P_{\text{artefact}} = 5.4 \text{ mJy}$

$P_{\text{source}} = 2 \text{ Jy}$

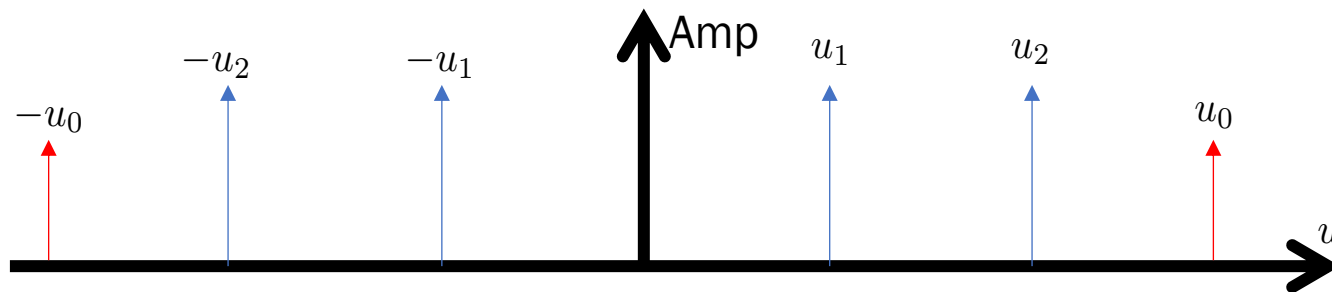
$$DR = \frac{P_{\text{source}}}{P_{\text{artefact}}} = \frac{2}{5.4 \times 10^{-3}} = 370$$

Drifts in antenna gains, +/- 1% amplitude error, max 1 degree phase error

Phase errors and dynamic range

- Let's take a simplified array - flat, linear array, N antennas
- Single integration observation of a point source - $N(N-1)/2$ visibilities
- Direction such that we only need to consider u axis
- Each baseline visibility is a δ spike in the uv plane
- All but one are 'perfect' (unit amplitude, zero phase)
- These have $V(u) = \delta(u - u_k)$ for the k th baseline.
- Phase error on baseline length u_0 of ϕ_ϵ radians so

$$V(u) = \delta(u - u_0) \exp(-i\phi_\epsilon)$$



Phase errors and dynamic range

- Image is formed by Fourier Transform:

$$I(l) = \int V(u) \exp(i2\pi ul) du$$

Each baseline contributes at position u_k and complex conjugate $-u_k$ in the visibility plane.

- Evaluating the term for each $(N(N-1)/2) - 1$ good baselines gives us $2 \cos(2\pi u_k l)$
- However single bad baseline gives $2 \cos(2\pi u_0 l - \phi_\epsilon)$
- Which, assuming small ϕ_ϵ gives: $\approx 2[\cos(2\pi u_0 l) + \phi_\epsilon \sin(2\pi u_0 l)]$
- So the image integral now becomes:

$$I(l) = 2\phi_\epsilon \sin(2\pi u_0 l) + 2 \sum_{k=1}^{N(N-1)/2} \cos(2\pi u_k l)$$

Phase errors and dynamic range

- The synthesised beam is (in this case):

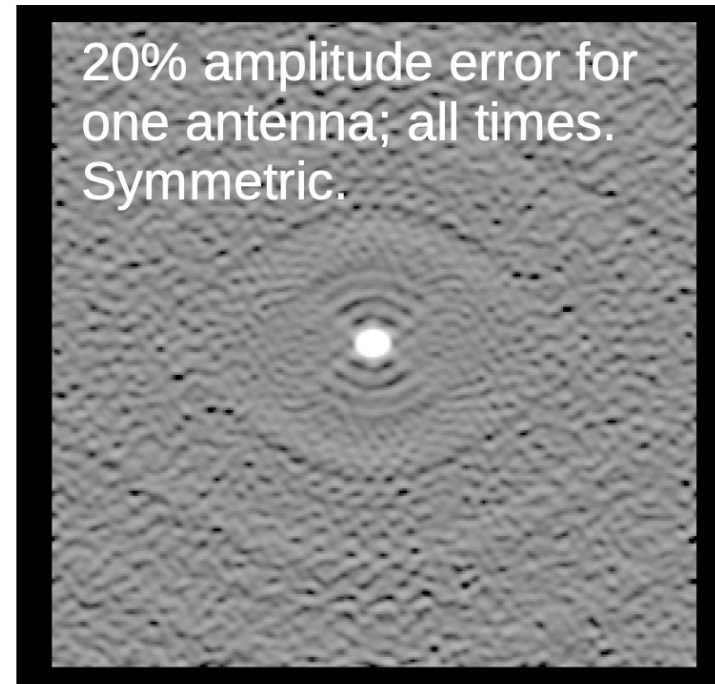
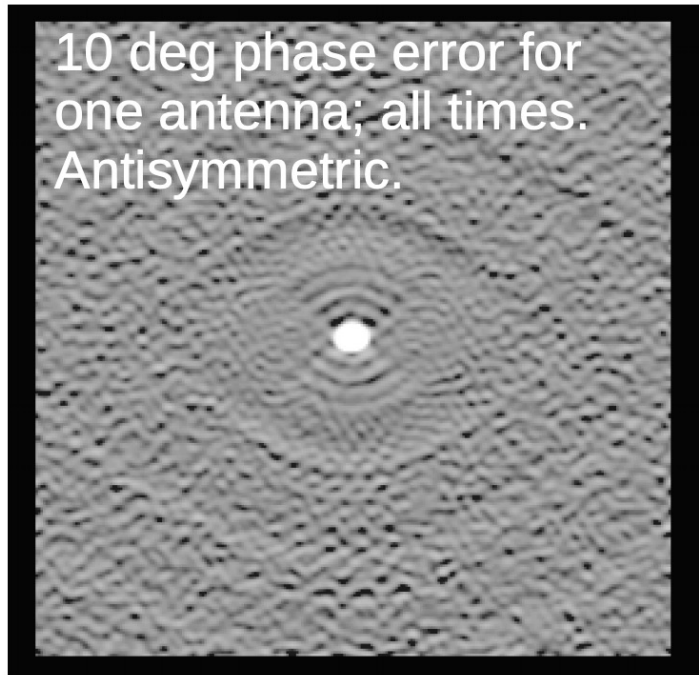
$$B(l) = 2 \sum_{k=1}^{N(N-1)/2} \cos(2\pi u_k l)$$

- Deconvolution is the subtraction of the beam from the image which leaves the residual error i.e.

$$\begin{aligned} R(l) = I(l) - B(l) &= \left[2\phi_\epsilon \sin(2\pi u_0 l) + 2 \sum_{k=1}^{N(N-1)/2} \cos(2\pi u_k l) \right] - 2 \sum_{k=1}^{N(N-1)/2} \cos(2\pi u_k l) \\ &= 2\phi_\epsilon \sin(2\pi u_0 l) \end{aligned}$$

- This is an ‘odd’ sinusoidal with amplitude $2\phi_\epsilon$ and period $1/u_0$

Phase errors and dynamic range



- A phase error of 10° is as bad as a 20% amplitude error
- Phase errors are sin (odd), amp are cos (even)

Phase errors and dynamic range

So far considered just one-baseline error, one integration:

- **All** baselines to one antenna affected by same error:
 - $(N - 1)$ bad baselines ($\sim N$ for large N)
 - $D_{\text{ant}} = D_B / (N - 1) = [N^2 / (N - 1)] / \sqrt{2} \phi_\epsilon \sim N / \sqrt{2} \phi_\epsilon$
- If **all** baselines are affected by **random noise**,
 - $D_{\text{all}} = D_B / \sqrt{N(N - 1)/2} = \sqrt{N(N - 1)/2} / \phi_\epsilon \sim N / \phi_\epsilon$

These expressions are valid if errors are correlated in time, e.g. single phase-ref scan, not much change in u (or v)

- For M periods (scans?) between which noise is uncorrelated:

Dynamic range is increased -

$$D_{\text{all}} \sim \sqrt{MN} / \phi_\epsilon$$

Phase errors and dynamic range

- Using this, lets take **10 antenna** array and **12 independent** scans
- All phase referencing applied, and well edited for RFI
- Typical residual phase scatter $\sim 20^\circ \rightarrow D_{\text{all}} \sim \sqrt{MN}/\phi_\epsilon \sim 100$

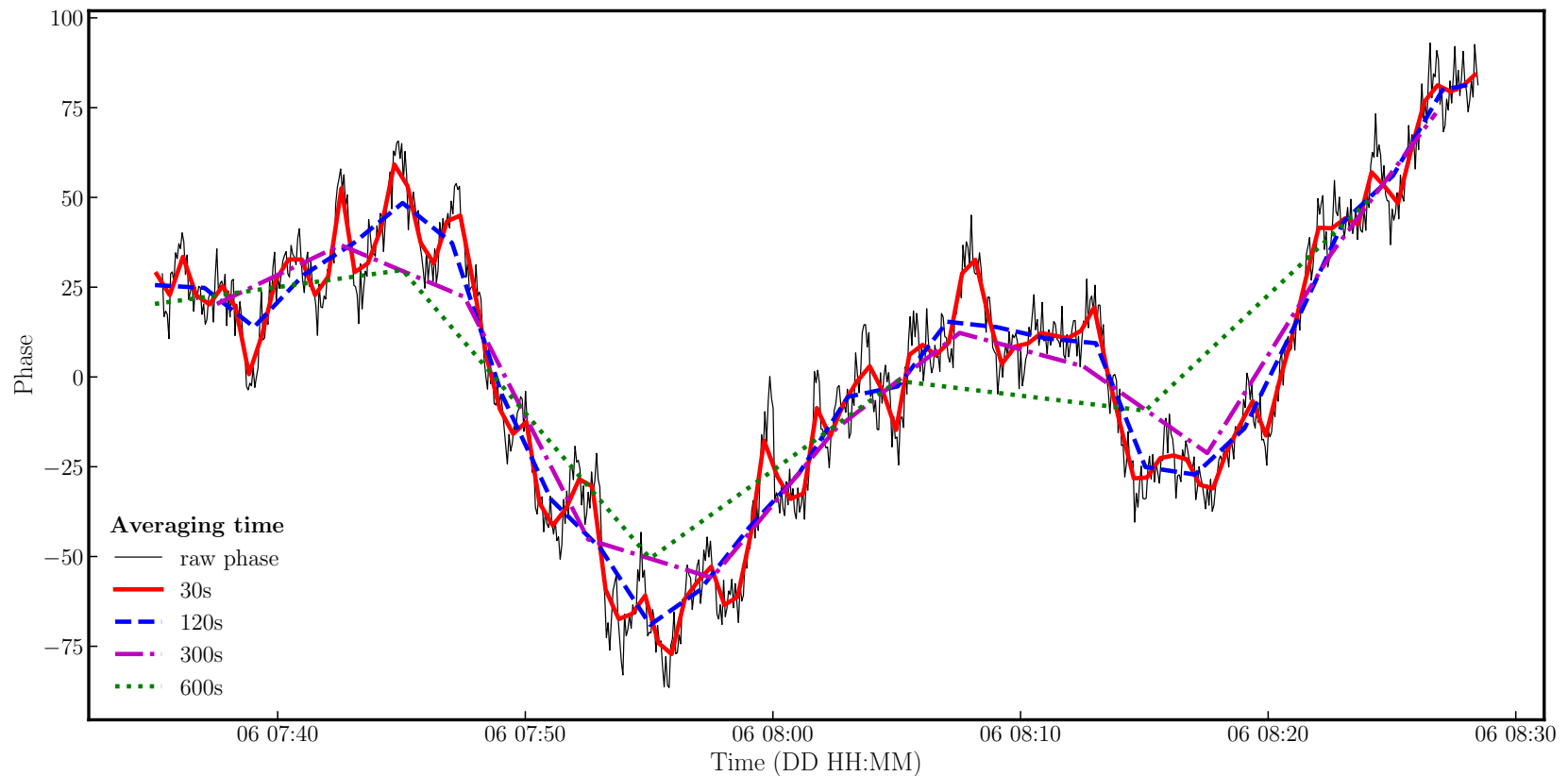
Can we improve on this?

- If map noise is near the T_{sys} limit and remaining errors are noise, then no!
- If noise is non-Gaussian and shows errors and well above T_{sys} limit then telescopes imperfectly calibrated so:
 - Use self-calibration per antenna, per scan (or longer) to get enough S/N so that the phase errors get below 20°

Solution intervals

Example phase variation across time

- Solution interval too long – lose phase structure
- Solution interval too short – not enough S/N unless very bright source



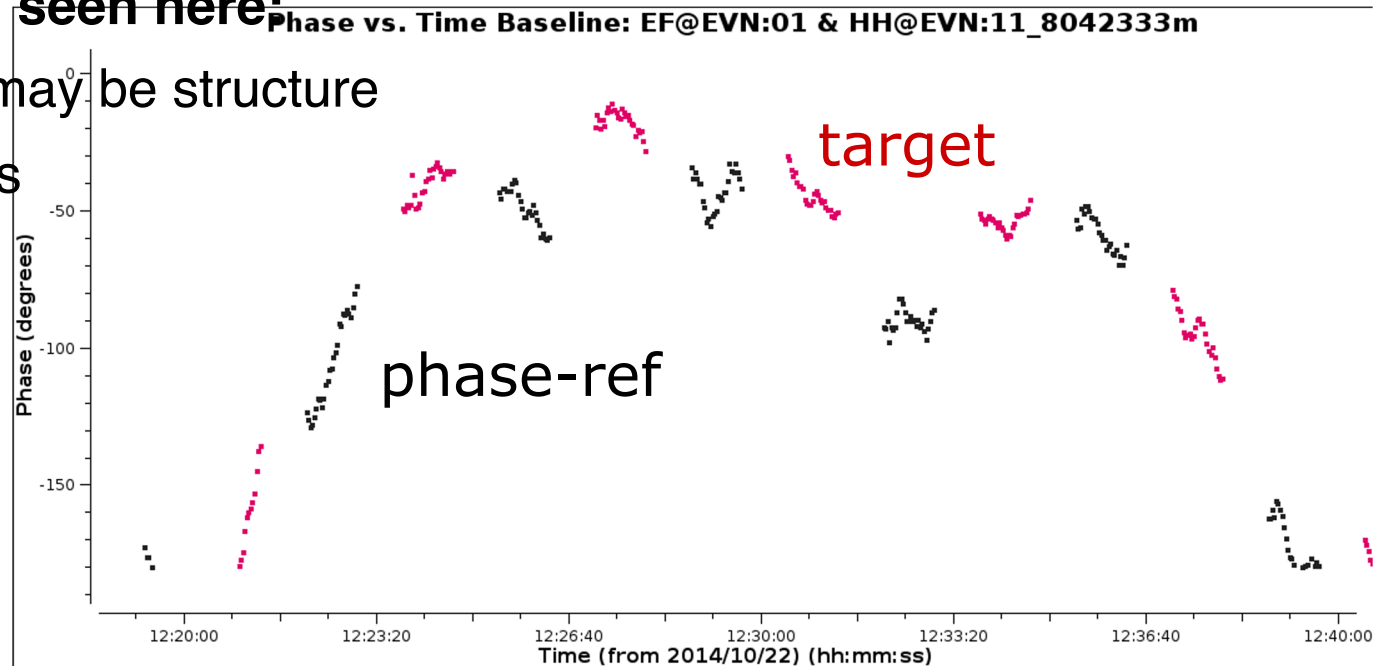
Time dependent phase calibration

Phase reference source:

- Need to interpolate solutions to target
- Does the phase-ref phase track the target phase?

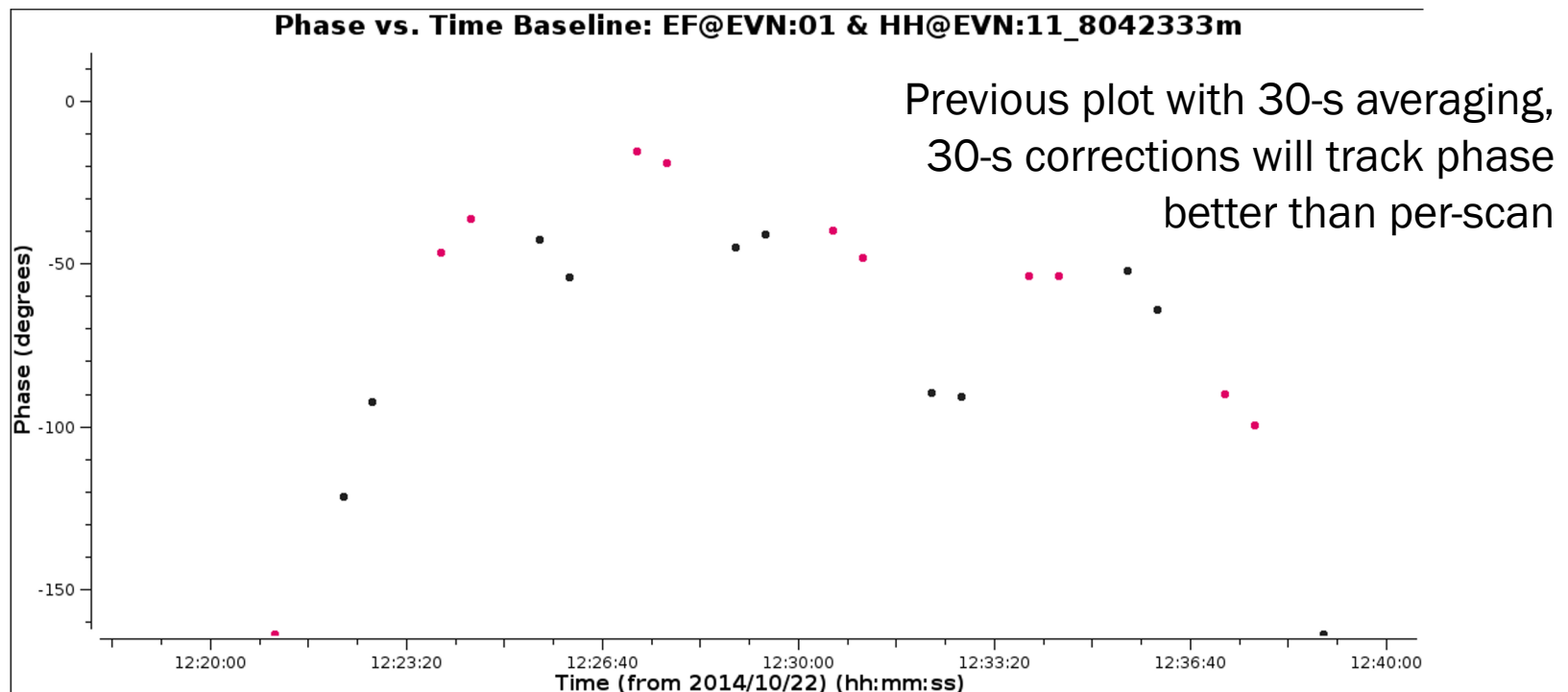
Consistent trend seen here:

- Target wiggles may be structure
- Some deviations



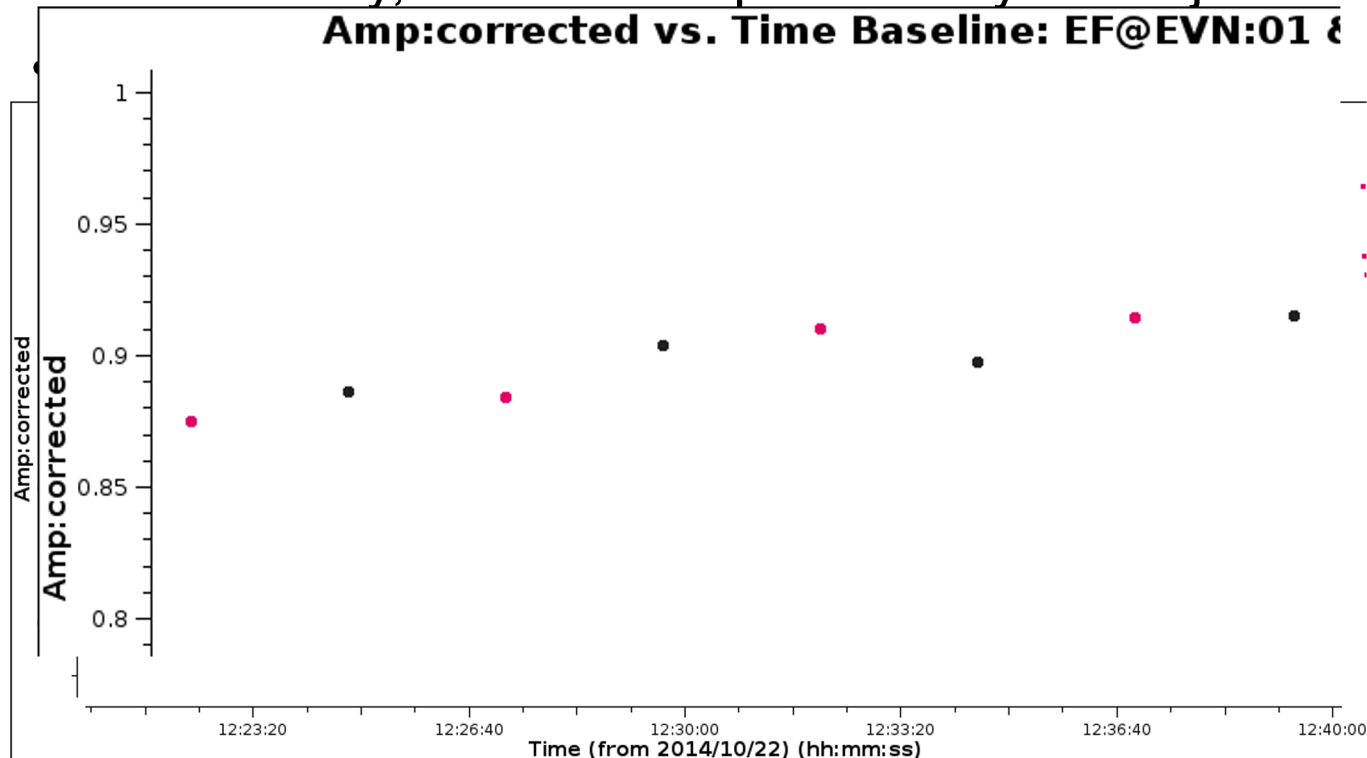
Time dependent phase calibration

- Need to interpolate phase-ref solutions to target
- Ideally no more than 2 solutions per phase-ref scan
- Check enough S/N in e.g. half scan
- Seeing low scatter by eye is OK!



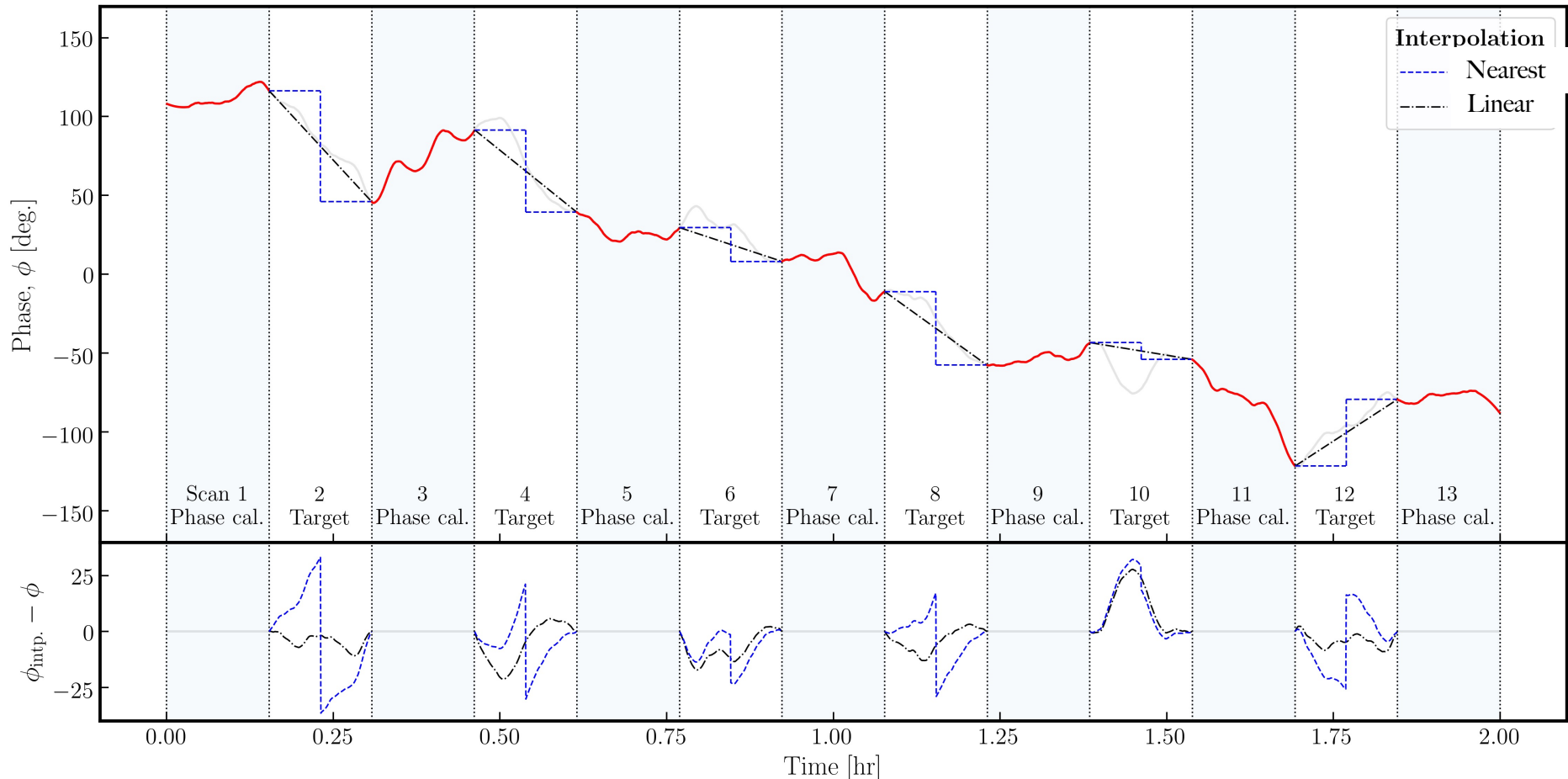
Time dependent amplitude calibration

- Apply phase solutions first to allow longer solint for amplitude calibration
- Avoid decorrelation
- If necessary, use shorter phase-only solint just for this



Interpolating solutions

- Interpolation chosen can increase calibration errors
- Linear is often better when extrapolating across scans



Conclusions

- “Good” calibration solution depend on the conditions of the observation and science goals
- Identify a good reference antenna
- Bandpass and amplitude solution intervals can be as long as possible to get best S/N
- Best solution interval for phase solutions depends, but almost always shorter than a single scan
- Want the best dynamic range possible – self calibration shall be shown to be very helpful in this respect!

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